ME303 Introduction to Mechanical Design

Lecture 13 Bearings, Lubrication, Brakes & Couplings

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Agenda

Week 12, Wednesday, Nov 27, 2019

- Bearing
 - Types
 - Life
 - Reliability
 - Load
 - Relating Concepts
 - Selection Design Assessment
 - Lubrication
 - Mounting & Enclosure

- Clutches & Brakes
 - Static Analysis
 - Types
 - Energy Considerations
 - Friction Materials
- Couplings



Rolling-Contact Bearing Types

The main load is transferred through elements in rolling contact.

• Most bearing manufacturers provide engineering manuals and brochures containing lavish descriptions of the various types available.





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(e)

Sealed

(j)

Self-aligning thrust

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All these bearings may be obtained with shields on one or both sides.

Types of Roller Bearings

What about the cost?

- Straight roller bearings
 - Carry a greater radial load than ball bearings of the same size because of the greater contact area.
 - Require almost perfect geometry of the raceways and rollers.
 - Straight roller bearings will not, of course, take thrust loads.
- Spherical-roller thrust bearing
 - Useful where heavy loads and misalignment occur.
 - The spherical elements have the advantage of increasing their contact area as the load is increased.
- Needle bearings
 - Useful where radial space is limited.
 - High load capacity
- Tapered roller bearings
 - Combine the advantages of ball and straight roller bearings.
 - High load-carrying capacity







- Straight roller
- Spherical roller, thrust









Steep-angle

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Bearing Life

A stochastic variable with both a distribution and associated statistical parameters.

- Common measures of Bearing Life
 - Number of revolutions of the inner ring (outer ring stationary) until the first tangible evidence of fatigue
 - Number of hours of use at a standard angular speed until the first tangible evidence of fatigue
- The life measure of an individual bearing
 - The total number of revolutions (or hours at a constant speed) of bearing operation until the failure criterion is developed.
- Failure criterion
 - Under ideal conditions, the fatigue failure consists of spalling of the load-carrying surfaces.
 - The spalling or pitting of an area of 0.01 in² (Timken Company)
- Rating Life (*Minimum life*, *L*₁₀ *life*, and *B*₁₀ *life*)
 - The number of revolutions (or hours at a constant speed) that 90 percent of a group of bearings will achieve or exceed before the failure criterion develops.
 - 10th percentile location of the bearing group's revolutions-to-failure distribution
 - Median Life (50th percentile), between $4\sim5$ times the L_{10} life.

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Bearing Load Life at Rated Reliability

What the manufacturing says vs. how long the bearings actually last

- To establish a single point, load F₁ and the rating life of group one (L₁₀)₁ are the coordinates that are logarithmically transformed.
- The **reliability** associated with this point, and all other points, is 0.90.
- Catalog load rating (C_{10})
- the radial load that causes 10 percent of a group of bearings to fail **at the bearing manufacturer's rating life**.



 $FL^{1/a} = \text{constant}$

• a = 3 for ball bearings

• a = 10/3 for roller bearings

Subsection of the section of the sec



Reliability versus Life

At constant load, the life measure distribution of rolling-contact bearings is right skewed.

- Three-parameter Weibull distribution
 - Robust ability to adjust to varying amounts of skewness
 - Used exclusively for expressing the reliability of rolling-contact bearings

• Reliability, *R*, for a Weibull distribution of the life measure

 x_0 = guaranteed, or "minimum," value of x

$$R = \exp\left[-\left(\frac{x-x_0}{\theta-x_0}\right)^b\right]$$

- θ = characteristic parameter. For rolling-contact bearings, this corresponds to the 63.2121 percentile value of *x*
- b = shape parameter that controls the skewness. For rolling-contact bearings, $b \approx 1.5$
- The life measure is expressed in dimensionless form as $x=L/L_{10}$.
- Given a specific required reliability, one can estimate life measure *x*. $x = x_0 + (\theta - x_0) \left(\ln \frac{1}{R} \right)^{1/b}$

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Relating Load, Life, and Reliability

A designer's problem

• What is desired (by the designer) is different from what is listed (by the manufacturer), so a compromise (decision) has to be made by the design engineer based on <u>an expected reliability</u>.

$$F_{B}x_{B}^{1/a} = F_{D}x_{D}^{1/a} \qquad R_{D} = \exp\left[-\left(\frac{x_{B} - x_{0}}{\theta - x_{0}}\right)^{b}\right]^{\log F}$$

$$x_{B} = x_{0} + (\theta - x_{0})\left(\ln\frac{1}{R_{D}}\right)^{1/b} \qquad c_{10}$$

$$F_{B} = F_{D}\left(\frac{x_{D}}{x_{B}}\right)^{1/a} = F_{D}\left[\frac{x_{D}}{x_{0} + (\theta - x_{0})[\ln(1/R_{D})]^{1/b}}\right]^{1/a}$$

an application factor a_f

$$\bullet C_{10} \approx a_f F_D \left[\frac{x_D}{x_0 + (\theta - x_0)(1 - R_D)^{1/b}} \right]^{1/a} R \ge 0.90$$

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A: The catalog information, the logs of C_{10} and $x_{10}=L_{10}/L_{10}=1$, a point on the 0.90 reliability contour.

D: The design point, a point on a desired reliability contour, $R=R_D$.

Moving from D through B to A.



Convert from a design situation with a desired load, life, and reliability to a catalog load rating based on a rating life at 90 percent reliability.



Combined Radial and Thrust Loading

A ball bearing is capable of resisting radial loading and a thrust loading, or combined.

- F_e to be the *equivalent radial load* that does the same damage as the combined radial (F_r) and thrust (F_a) loads together.
- A *rotation factor* V is defined such that V=1 when the inner ring rotates and V=1.2 when the outer ring rotates.
 - For the case of ball bearing
- Two dimensionless groups can be plotted.
 - $F_e / (VF_r)$ and $F_a / (VF_r)$
 - The abscissa *e* is the intersection
- Expression $F_e = X_i V F_r + Y_i F_a$
 - where i = 1 when $F_e / (VF_r) \le e$
 - and i = 2 when $F_a / (VF_r) > e$.



Equivalent Radial Load Factors for Ball Bearings The X and Y factors depend upon the geometry and construction of the specific bearing.

		$F_a/(VF_r) \leq e$		$F_a/(VF_r) > e$	
F_{a}/C_{0}	е	X 1	Y ₁	X 2	Y ₂
0.014*	0.19	1.00	0	0.56	2.30
0.021	0.21	1.00	0	0.56	2.15
0.028	0.22	1.00	0	0.56	1.99
0.042	0.24	1.00	0	0.56	1.85
0.056	0.26	1.00	0	0.56	1.71
0.070	0.27	1.00	0	0.56	1.63
0.084	0.28	1.00	0	0.56	1.55
0.110	0.30	1.00	0	0.56	1.45
0.17	0.34	1.00	0	0.56	1.31
0.28	0.38	1.00	0	0.56	1.15
0.42	0.42	1.00	0	0.56	1.04
0.56	0.44	1.00	0	0.56	1.00
*Use 0.014 if F _a	$C_0 < 0.014.$	F	$T_e = X_i V F_r$	$+ Y_i F_a$	



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Notes on Bearing Selection

What's available from the manufacturer's handbook?

- Such information has been accumulated the hard way, that is, by experience.
- The beginner designer should utilize this information until he or she gains enough experience to know when deviations are possible.

Type of Application	Life, kh	Type of Application	Loc	ıd Factor
Instruments and apparatus for infrequent use	Up to 0.5	Precision gearing		1.0-1.1
Aircraft engines	0.5-2	Commercial gearing		1.1–1.3
Machines for short or intermittent operation where service		Applications with poor bearing sea	lls	1.2
interruption is of minor importance	4-8	Machinery with no impact		1.0-1.2
Machines for intermittent service where reliable operation		Machinery with light impact		1.2–1.5
is of great importance	8-14	Machinery with moderate impact		1.5-3.0
Machines for 8-h service that are not always fully utilized	14-20			OF SCIEMA
Machines for 8-h service that are fully utilized	20-30	Bearing-Life	Load-Application	
Machines for continuous 24-h service	50-60	Recommendations	Factors, same	HUNDER WEIGHT
Machines for continuous 24-h service where reliability is of extreme importance	100-200	for Various Classes of Machinery	purpose as the factors of safety.	SUSTech Southern University

Example on Bearing Life Estimation

An SKF 6210 angular-contact ball bearing has an axial load F_a of 400 lbf and a radial load F_r of 500 lbf applied with the outer ring stationary. The basic static load rating C_0 is 4450 lbf and the basic load rating C_{10} is 7900 lbf. Estimate the \mathcal{L}_{10} life at a speed of 720 rev/min.

F_a/C_0	е	
0.084	0.28	
0.090	е	from which $e = 0.285$
0.110	0.30	
$F_a/(VF_r)$) = 400/[[(1)500] = 0.8 > 0.285.
W/:+1	· (P _	φ and $E = E$
with	$\mathcal{L}_D = \mathcal{L}_D$	\mathfrak{X}_{10} and $\mathfrak{F}_D = \mathfrak{F}_e$,

V = 1 and $F_a/C_0 = 400/4450 = 0.090$.

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60(720) \890.8/

Lubrication

The contacting surfaces in rolling bearings have a relative motion that is both rolling and sliding, so it is difficult to understand exactly what happens.

• The purposes of an antifriction-bearing lubricant:

- To provide a film of lubricant between the sliding and rolling surfaces 1.
- 2. To help distribute and dissipate heat
- To prevent corrosion of the bearing surfaces 3.
- 4. To protect the parts from the entrance of foreign matter

Use Grease When Use Oil When 1. The temperature is not over 200°F. 1. Speeds are high. 2. The speed is low. 2. Temperatures are high.

- 3. Unusual protection is required from the entrance of foreign matter.
- 4. Simple bearing enclosures are desired.
- 5. Operation for long periods without attention is desired.

- 3. Oiltight seals are readily employed.
- 4. Bearing type is not suitable for grease lubrication.
- 5. The bearing is lubricated from a central supply which is also used for other machine parts.



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Mounting and Enclosure

Each new design is a real challenge to the ingenuity of the designer.

• Each operation contributes to the cost of production, so that the designer, in ferreting out a trouble-free and low-cost mounting, is faced with a difficult and important problem



Clutches, Brakes, Couplings, and Flywheels

Rotary elements with the function of storing and/or transferring rotational energy.

- Interest of analysis
 - The actuating force
 - The torque transmitted
 - The energy loss
 - The temperature rise
- Types
 - Rim types with internal expanding shoes
 - Rim types with external contracting shoes
 - Band types
 - Disk or axial types
 - Cone types
 - Miscellaneous types

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Static Analysis of Clutches and Brakes

Similar Procedure of Analysis

- Estimate, model, or measure the pressure distribution on the friction surfaces.
- Find a relationship between the largest pressure and the pressure at any point.
- Use the conditions of static equilibrium to find the braking force or torque and the support reactions.



How A Clutch Works?

https://www.youtube.com/watch?v=pqF-aBtTBnY





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Internal Expanding Rim Clutches and Brakes

- Three essential elements
 - the mating frictional surface,
 - the means of transmitting the torque to and from the surfaces,
 - and the actuating mechanism.



- Clutch classification based on operating mechanism
 - Expanding-ring
 - often used in textile machinery, excavators, and machine tools where the clutch may be located within the driving pulley
 - Centrifugal
 - used mostly for automatic operation
 - Magnetic
 - particularly useful for automatic and remote-control systems
 - Hydraulic & Pneumatic
 - useful in drives having complex loading cycles and in automatic machinery, or in robots



External Contracting Rim Clutches and Brakes

- Operating mechanisms can be classified as
 - Solenoids
 - Levers, linkages, or toggle devices
 - Linkages with spring loading
 - Hydraulic and pneumatic devices





An external contracting clutchbrake that is engaged by expanding the flexible tube with compressed air.

> SUSTech Southern University of Science and Technology

Disk Brakes

No fundamental difference between a disk clutch and a disk brake

- The caliper supports a single floating piston actuated by hydraulic pressure.
- Caliper brakes (named for the nature of the actuating linkage) and disk brakes (named for the shape of the unlined surface) press friction material against the face(s) of a rotating disk.



Energy Considerations

the amount of heat generated by a clutching or braking operation

- Heat generation
 - When the rotating members of a machine are caused to stop by means of a brake, the kinetic energy of rotation must be absorbed by the brake.
 - When the members of a machine that are initially at rest are brought up to speed, slipping must occur in the clutch until the driven members have the same speed as the driver.
- The character of the load may be such that, if this torque value is permitted, the clutch or brake may be destroyed by its own generated heat.
 - the characteristics of the material
 - the ability of the clutch to dissipate heat

We assume that the two shafts are rigid and that the $I_1 \overset{I_1}{\Theta}_1 = -T$ $\dot{\theta} = \dot{\theta}_1 - \dot{\theta}_2 = -\frac{T}{I_1}t + \omega_1 - \left(\frac{T}{I_2}t + \omega_2\right)$ $I_2 \overset{\Box}{\Theta}_2 = T$ $= \omega_1 - \omega_2 - T\left(\frac{I_1 + I_2}{I_1I_2}\right)t$

Clutch or brake

Let the time required for the entire operation be t_1 .

$$\dot{\theta} = 0$$
 when $\dot{\theta}_1 = \dot{\theta}_2$, $t_1 = \frac{I_1 I_2 (\omega_1 - \omega_2)}{T(I_1 + I_2)}$

$$u = T\dot{\theta} = T\left[\omega_1 - \omega_2 - T\left(\frac{I_1 + I_2}{I_1 I_2}\right)t\right]$$

$$E = \int_{0}^{t_{1}} u \, dt = T \int_{0}^{t_{1}} \left[\omega_{1} - \omega_{2} - T \left(\frac{I_{1} + I_{2}}{I_{1}I_{2}} \right) t \right] dt$$
$$= \frac{I_{1}I_{2}(\omega_{1} - \omega_{2})^{2}}{2(I_{1} + I_{2})}$$



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Friction Materials

The manufacture of friction materials is a highly specialized process, and it is advisable to consult manufacturers' catalogs and handbooks, as well as manufacturers directly, in selecting friction materials for specific applications.

- High and reproducible coefficient of friction
- Imperviousness to environmental conditions, such as moisture
- The ability to withstand high temperatures, together with good thermal conductivity and diffusivity, as well as high specific heat capacity
- Good resiliency
- High resistance to wear, scoring, and galling
- Compatible with the environment
- Flexibility

	Friction	Maximum	Maximum Temperature		Maximum	
Material	Coefficient f	Pressure p _{max} , psi	Instantaneous, °F	Continuous, °F	Velocity V _{max} , ft/min	Applications
Cermet	0.32	150	1500	750		Brakes and clutches
Sintered metal (dry)	0.29-0.33	300-400	930-1020	570-660	3600	Clutches and caliper disk brakes
Sintered metal (wet)	0.06-0.08	500	930	570	3600	Clutches
Rigid molded asbestos (dry)	0.35-0.41	100	660–750	350	3600	Drum brakes and clutches
Rigid molded asbestos (wet)	0.06	300	660	350	3600	Industrial clutches
Rigid molded asbestos pads	0.31-0.49	750	930-1380	440-660	4800	Disk brakes
Rigid molded nonasbestos	0.33-0.63	100-150		500-750	4800-7500	Clutches and brakes
Semirigid molded asbestos	0.37-0.41	100	660	300	3600	Clutches and brakes
Flexible molded asbestos	0.39-0.45	100	660-750	300-350	3600	Clutches and brakes
Wound asbestos yarn and wire	0.38	100	660	300	3600	Vehicle clutches
Woven asbestos yarn and wire	0.38	100	500	260	3600	Industrial clutches and brakes
Woven cotton	0.47	100	230	170	3600	Industrial clutches and brakes
Resilient paper (wet)	0.09-0.15	400	300		$PV < 500 \ 000$	Clutches and transmission
Characteristics of Friction Materials for Brakes and Clutches psi · ft/min bands						

Miscellaneous Clutches and Couplings

- Design Considerations
 - They do not slip.

- No heat is generated.
- They cannot be engaged at high speeds.
- Sometimes they cannot be engaged when both shafts are at rest.
- Engagement at any speed is accompanied by shock.
- The greatest differences among the various types of positive clutches are concerned with the design of the jaws.



Project 3: Shaft Design

• Online at course website

Next class

- Lab for Group 1: Design Consultation
- Friday 0800-1000, Nov 29
- Room 412, 5 Wisdom Valley
- **Discussion for Group 2**: Design Consultation
- Friday 0800-1000, Nov 29
- Room 202, 1 Lychee Park

Thank you!

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